

AERODYNAMIC FLOW CONTROL

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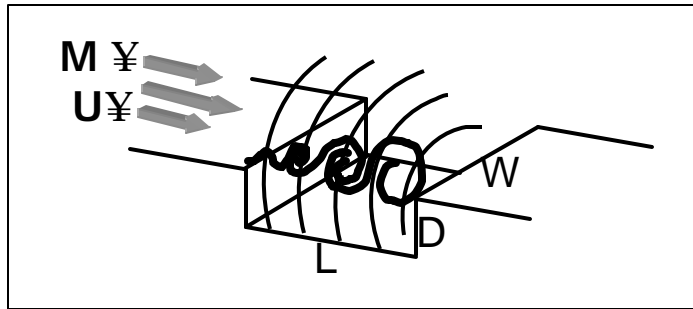
Outline



- **Examples of VA Efforts (AIAA Paper 2004-2622)**
- **What is flow control?**
- **Low-order model approach (KISS)**
 - **Pitching airfoil**
 - **Cavity tone suppression**
 - **Separation control**
- **Reduced-order model approach (KIRS)**
 - **Nonlinear convection**
- **Summary and future work**



Cavity Flow Control





HIFEX Test at ARA

Objective of Research:

Compare the effectiveness of high- and low-frequency flow control methodologies and applied them to a generic weapons bay

Test Conditions

- Mach 0.85 and 1.19

Devices Tested

- One-Delta “Sawtooth” Spoiler
- Pulse-blowing “Rotary” Actuator
- Power Resonance Tube (PRT) and Splash Jet
- Rod and Rod with Wire



HIFEX Model

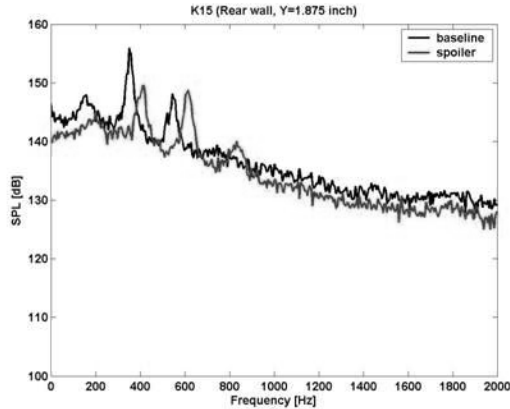
- 10% Scale Weapons Bay Model
- Dimensions 20” x 4” x 4”
- L/D = 5
- Attached Doors Positioned at 90°



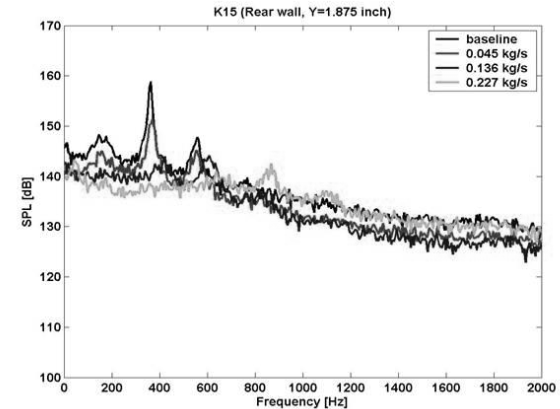
Results of HIFEX Test



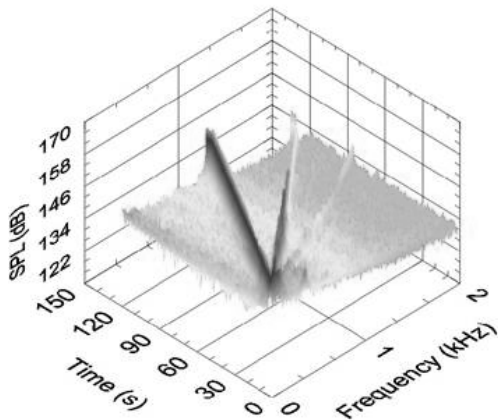
Passive “Zero-Frequency” Actuation



High-Frequency Actuation > 1 kHz



Low-Frequency Actuation < 1 kHz



Frequency Sweep of Device

	Zero-Frequency		Low-Frequency		High-Frequency	
	Tonal	OASPL	Tonal	OASPL	Tonal	OASPL
Subsonic	6 dB	3.5 dB	17 dB 14 dB	5 dB 2 dB	34 dB (PRT)	8.5 dB (PRT/S. Jet)
Supersonic	1 dB	2.0 dB	18 dB 19 dB	9 dB 8.5 dB	34 dB (S. Jet)	14 dB (PRT/S. Jet)

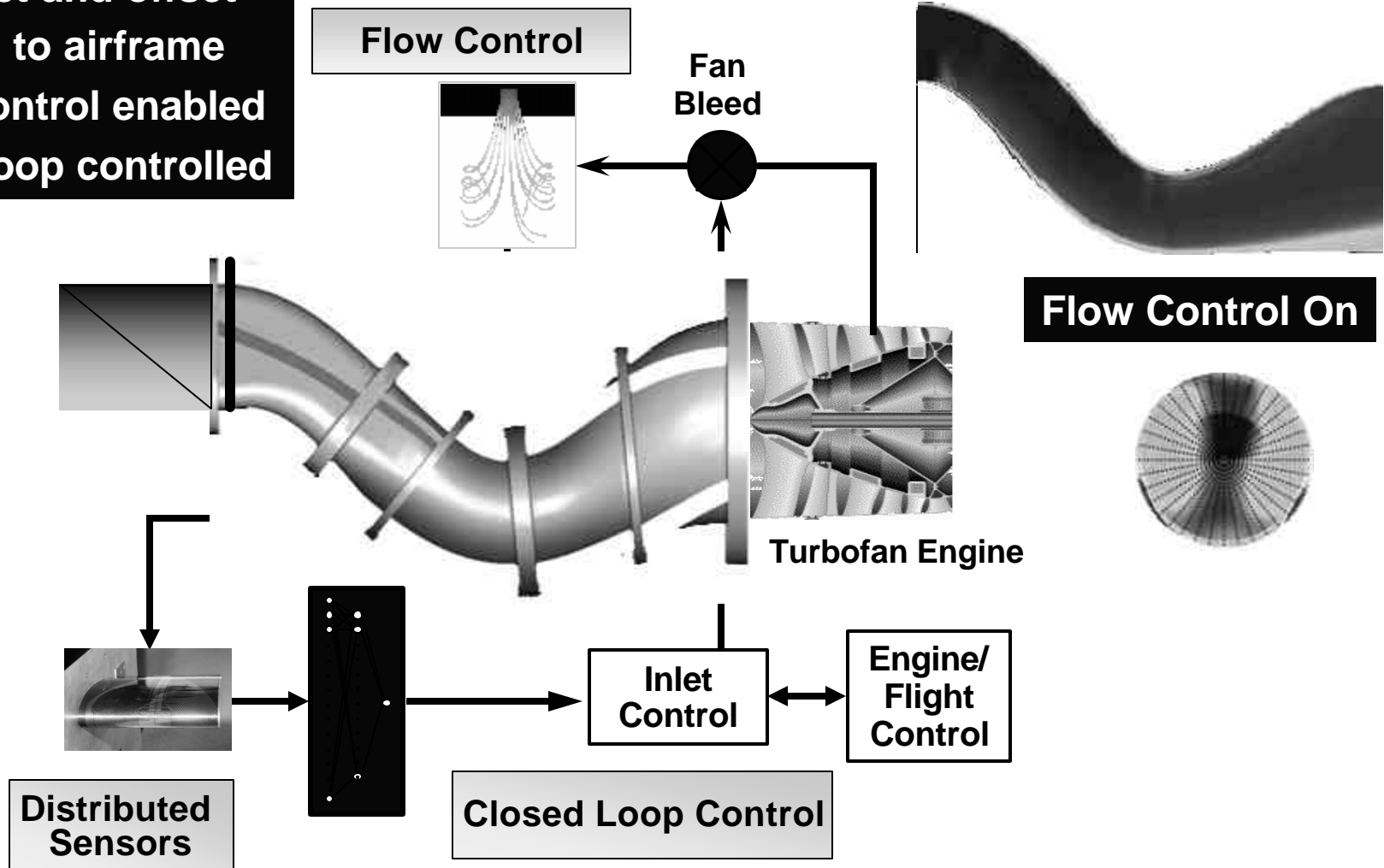
High-Frequency Actuation (PRT/ Splash Jet) Reduces Tonal Peak and OASPL better than any other method tested.



Active Integrated Inlets

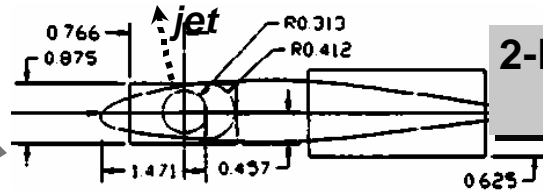


- Compact and offset
- Integral to airframe
- Flow-control enabled
- Close-loop controlled



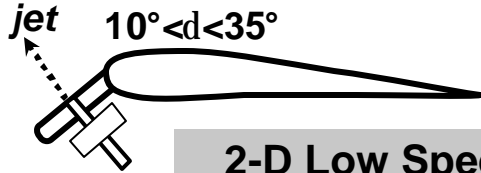


Pulsed Vortex Generator Jets

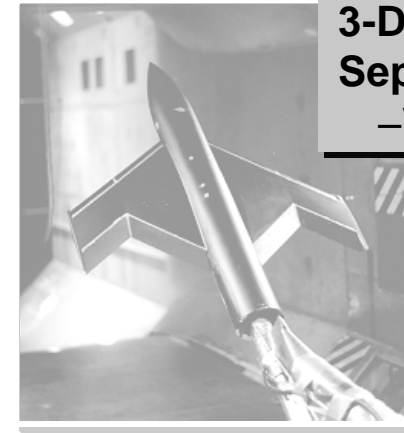


2-D Compressible Validation

- $M=0.3-0.7$
- $C_{l,max}$ inc. 21-14%
- L/D inc. up to 35%

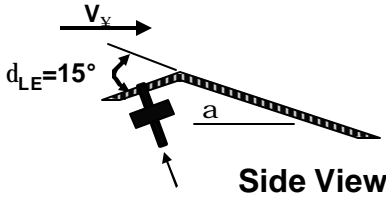


2-D Low Speed Separation Control

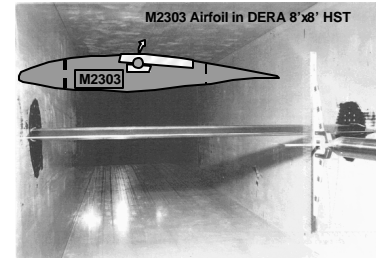
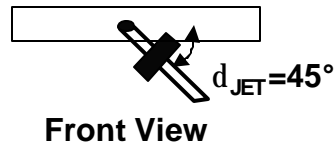


3-D Low Speed Separation Control - Vehicle Control

- $M=0.1&0.2$
- $C_{L,max}$ inc. 7%
- L/D inc. up to 17%
- Prop. roll control



2-D Low Speed Exploration



- $M=0.67-0.71$
- $Re_c=19 \times 10^6$
- $F^+ = f(x_{te}-x_{jet}) / V_{\infty} \gg 0.6-0.8$
- Overall L/D increase over high-a range



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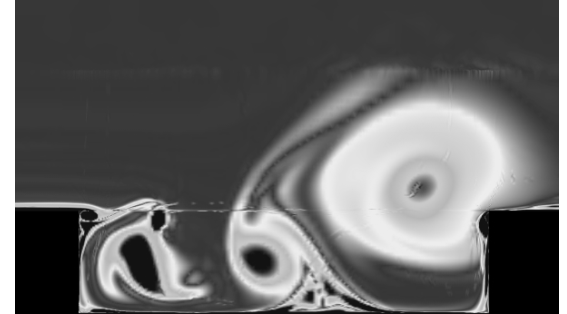


Defining Flow Control



Do you know what “control” means?

- **Passive flow control**
 - Modifications to geometry
- **Active flow control**
 - Adding/removing mass, momentum, or energy to the flow, e.g. synthetic jets, pulsed vortex generators, mass injection, suction
- **Quasi-steady** – Slow relative to time scales of fluid
 - Active flow control with monitoring and updating of control input, e.g. performance enhancement
- ***Feedback flow control***
 - *Feedback control theory applied to active flow control*
 - *Time scales for control on order of time scales of the system*

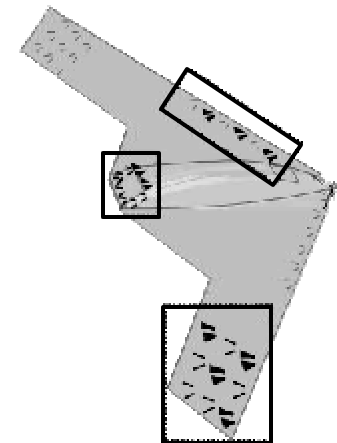
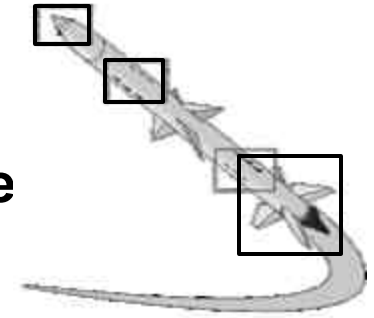




Motivation



- **Ability of small-scale devices to effect large-scale changes in aerodynamic flows through natural amplification has been demonstrated**
 - Open-loop
- **Ability to control flow fields by sensing their state the employing these mechanisms is within reach**
- **Goal — integrate aerodynamic flow control techniques with closed-loop control theory**
- **Potential applications**
 - Replacements for traditional aircraft control surfaces
 - Weapons bay acoustics
 - Drag reduction

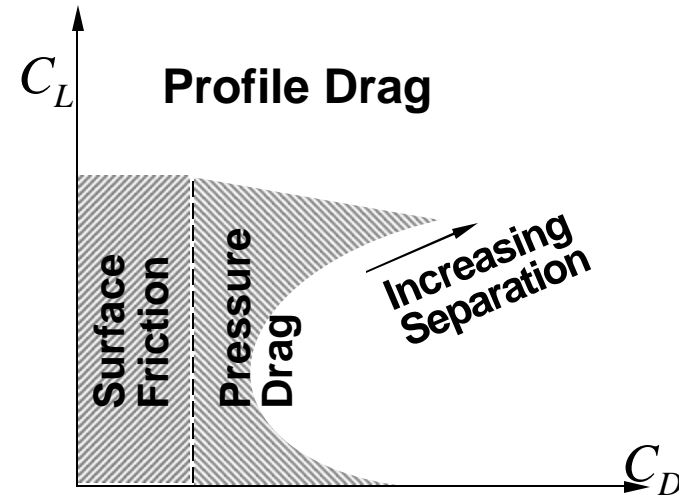




Why Is It A Difficult Problem?

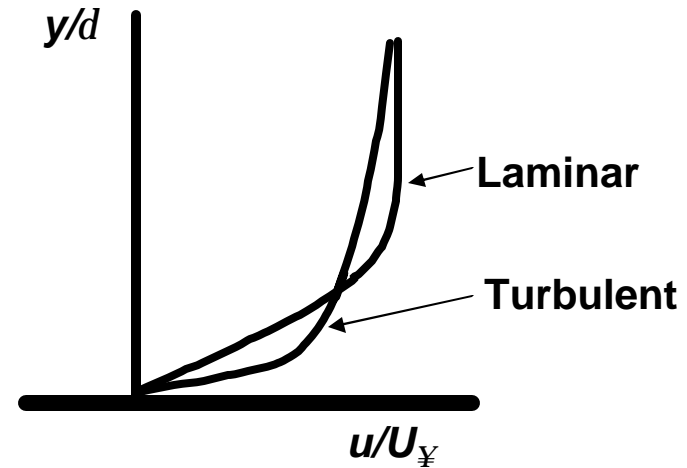
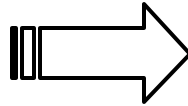
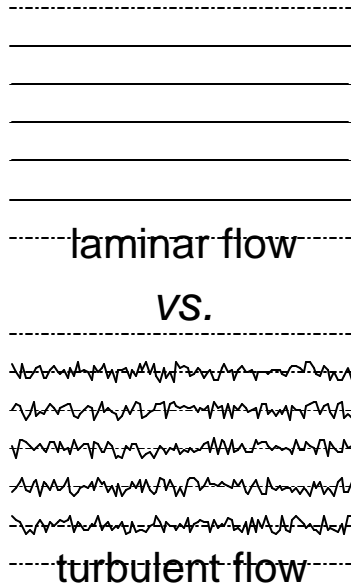


- **Components of drag**
 - Trailing vortices, lift generation
 - Friction
 - Lack of pressure recovery at T.E., wake
 - Separation (makes pressure recovery worse)
 - Wave (shock - transonic and supersonic)





Re-laminarization Reduces Drag



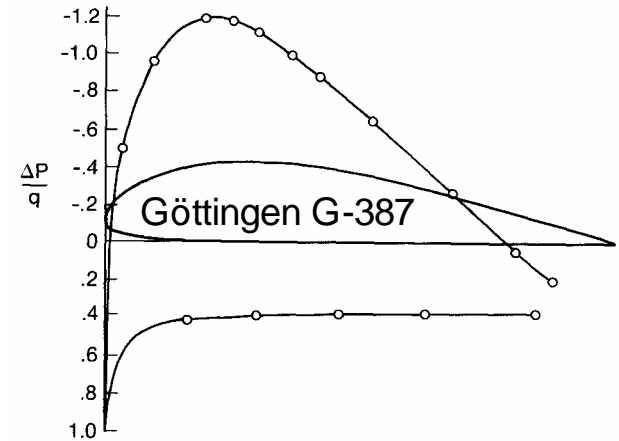
- Friction drag is proportional to velocity gradient at wall: $t_w = \mu \left(\frac{\partial u}{\partial y} \right)_{y=0}$
- Laminar flow has less mixing of far-field with flow near wall
→ smaller velocity gradient



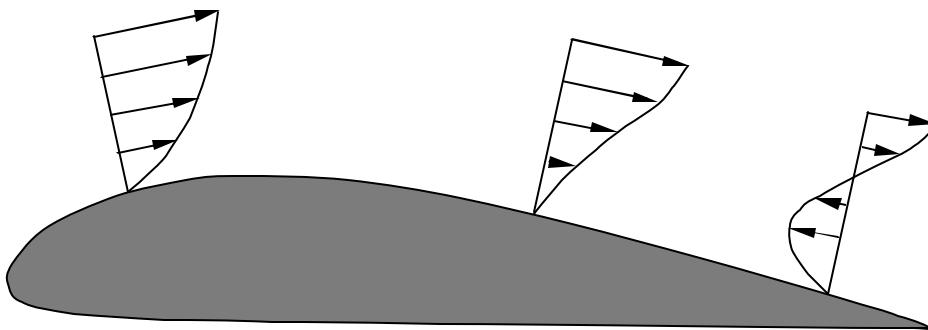
Likelihood of Separation Increased



- Adverse pressure gradient retards the flow
- Separation occurs where
- Separation occurs farther downstream in turbulent flow due to increased mixing of high velocity fluid in far-field with low velocity fluid near the surface



from Jones, Robert T., *Wing Theory*, Princeton University Press, Princeton, NJ, p. 36.



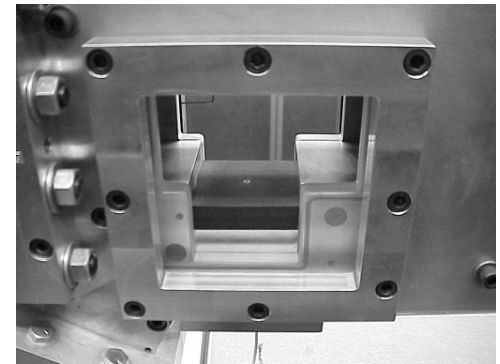
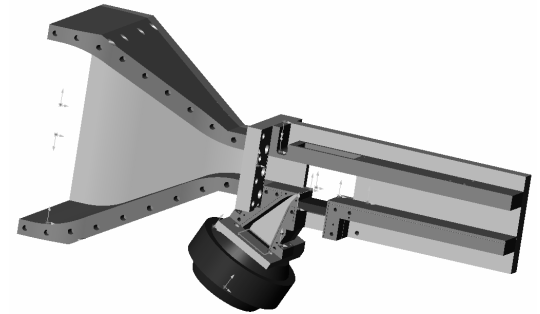
from Brown, F.N.M., *See the Wind Blow*, 1971, plate. 42.



Role of Feedback in Flow Control



- **General role of feedback**
 - **Stabilization**
 - **Tracking in presence of uncertainty**
- **Necessary components for model-based approaches**
 - **Model that captures dynamics of relationships between inputs (actuators), outputs (variables to be controlled)**
 - **Definition of states (not trivial in flow control)**
 - **Quantified control objective (not trivial)**



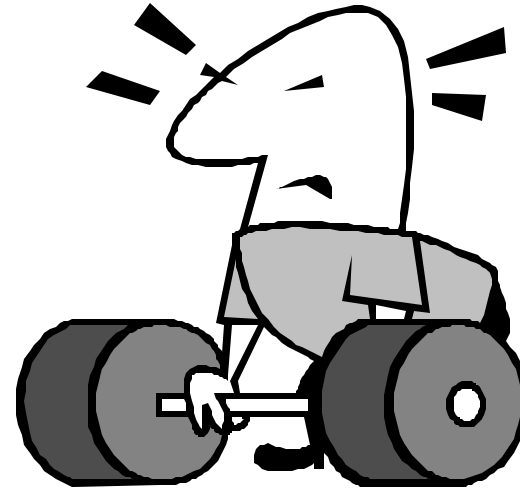


Technical Challenges/Approaches



- **Technical Challenges**

- Actuation devices and power
- Feedback sensing
- Flow physics
- **Order reduction for models**
- **Control law design**
- **Order reduction of control**



- **Approaches**

- “**Experimental**” data collection with low-order model → **Control design**
- **Simulation and reduction of model order** → **Control design**
- Control of PDE → Order reduction

Increasing application ↑

↑
Increasing generality ↓



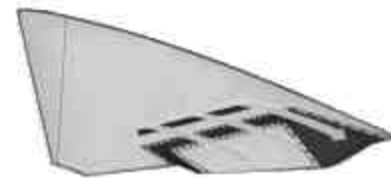
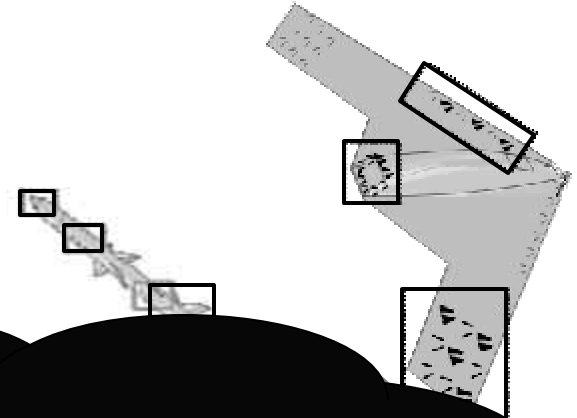
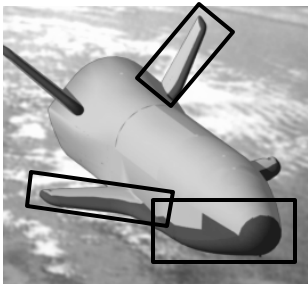
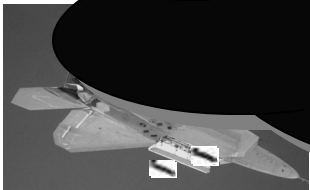
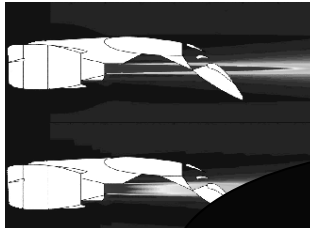
Air Vehicle Applications for Flow Control



- **Vehicle control**
- **Separation control**
- **Aero-acoustic fatigue**
- **Skin friction reduction**
- **Thermal**

Which applications will benefit from order reduction and feedback control?

- **Noise attenuation**
- **Buffet alleviation**
- **Pressure distortion**
- **Compressor, turbine, combustor control**

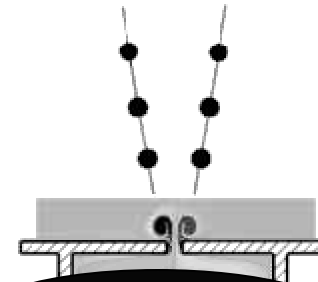




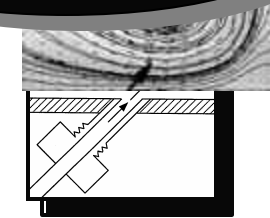
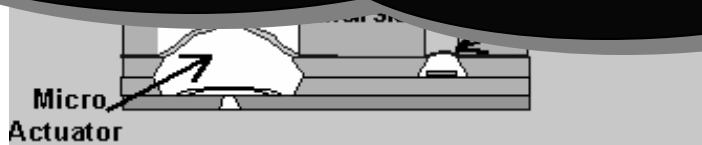
Actuators & Sensors



- Many choices for actuators and sensors
- Actuators – must be amenable to simulation/modeling
 - Synthetic jets (MEMS and non-MEMS)
 - Pulsed vortex generator jets
 - Deployable vortex generators
 - Pulsed/steady blowing/suction
- Sensors



Which actuators are relevant for order reduction and control law design?





Ranges of Actuators



Macro Devices

Micro Devices

Passive



Active

Macro Vanes

Sub Boundary Layer VGs

P-DRE

Fluidic Shape Change

Pulsed Injection & VG Jets

Oscillatory Zero Net Mass Flux

Open-Loop Near Wall

Synthetic/Micro Jets

Reactive Near Wall

Mechanical Deployables: VGs, roughness, bubbles

FlexSys Inc.

Orbital Research Inc.

BOEING

N&A

Global Generators



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Control of Wing Attitude with Synthetic Jets



- **Goal: Vehicle control without hinged moving surfaces**
- **Objective: Develop feedback flow control methods for vehicle control**
- **Technical Challenges:**
 - **Modeling of input/output relationships**
 - **Must be amenable to control law design**
 - **Must be valid for wide range of operating conditions**
 - **Control law design**
 - **Nonlinearities in system**
 - **Imperfect models**
 - **Efficient actuators with sufficient control authority over wide operating range**
- **Approach: Develop system for pitching/plunging 2D airfoil in wind tunnel with low-order models**

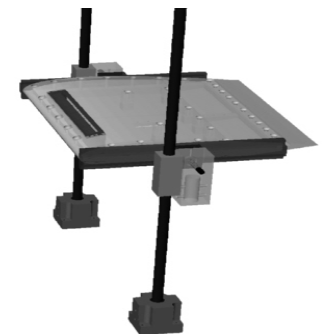
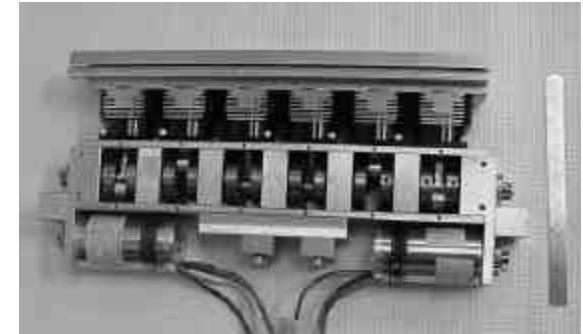
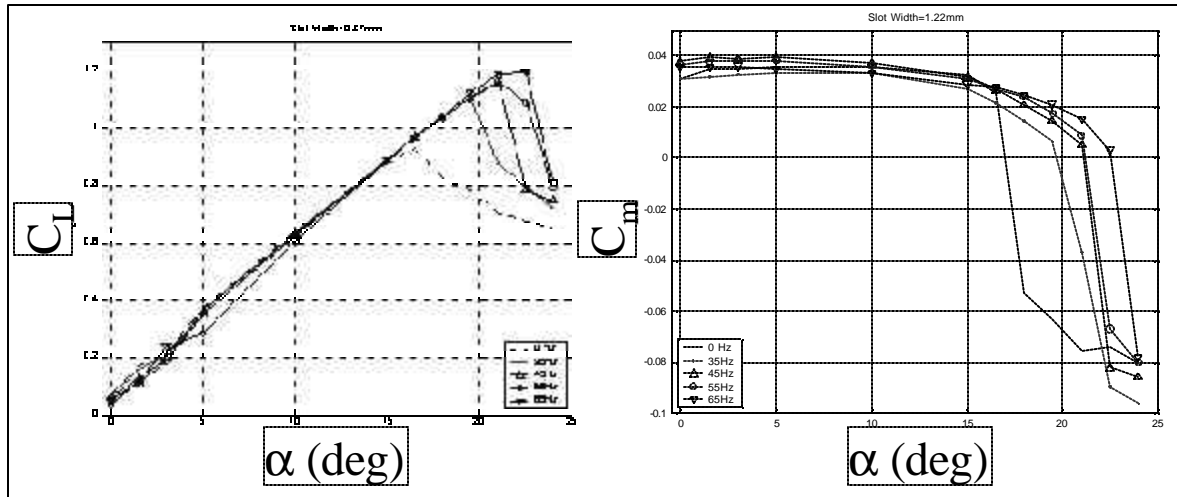




Leading Edge Control with Flow Separation



- Control of the forces/moments possible at high angle of attack by controlling separation
 - Array of six piston/cylinder synthetic jets near leading edge
 - Good control authority above stall (17 deg angle of attack)
 - Nonlinear relationship between synthetic jet frequency, angle of attack, and lift and pitching moment

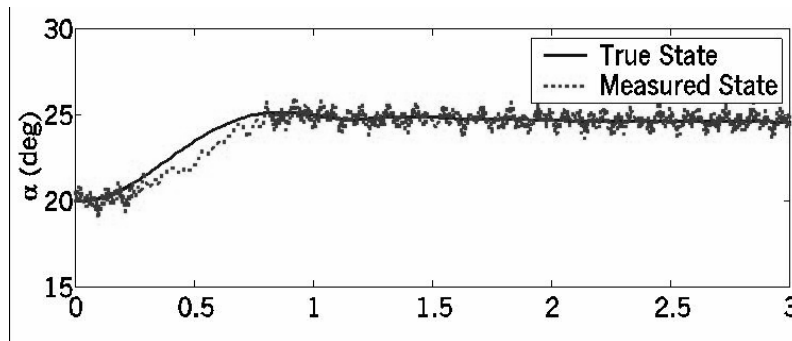




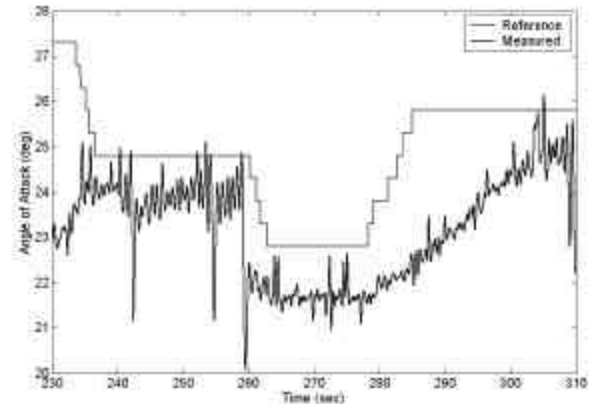
Demonstration of Pitch Control via Feedback Flow Control



- Control law tested in simulation
- Feedback control of angle of attack demonstrated in wind tunnel
 - Via control of reattachment of separated flow



Simulation Results



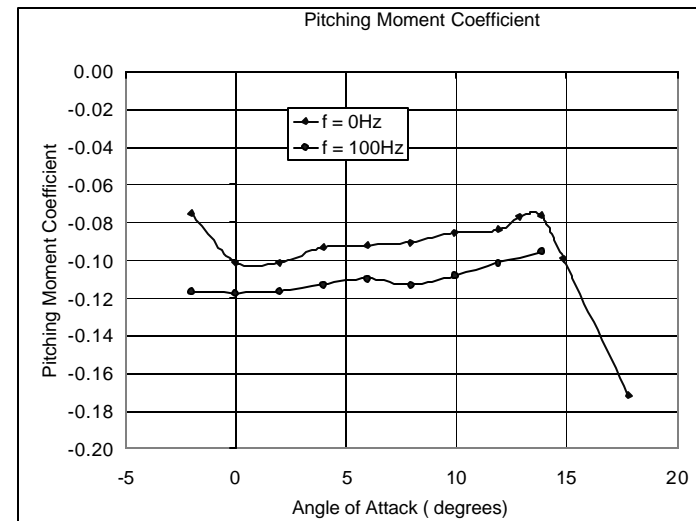
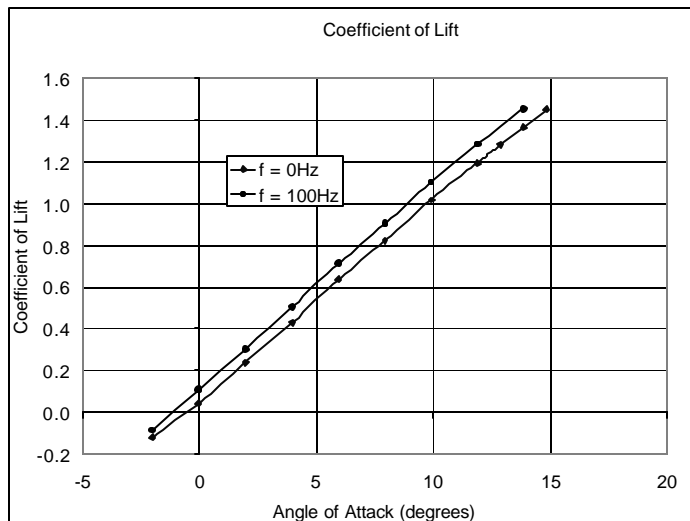
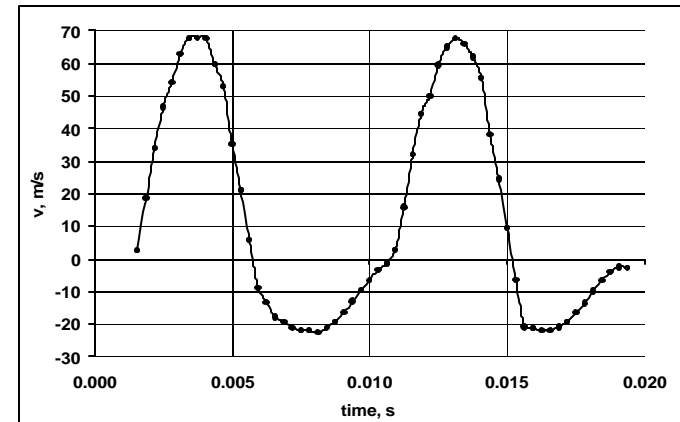
Experimental Results



Trailing Edge Control for Low Angles of Attack

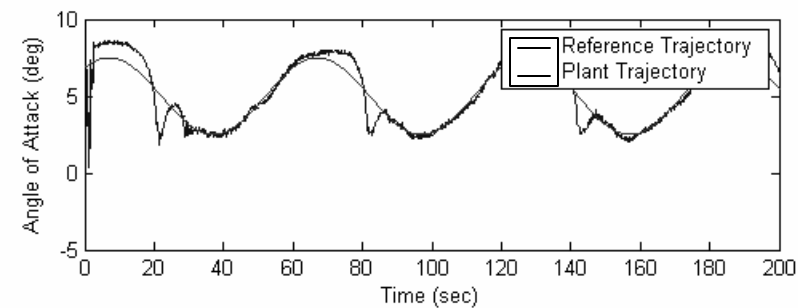
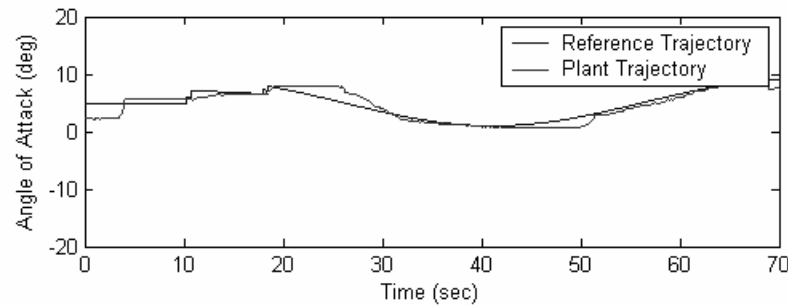
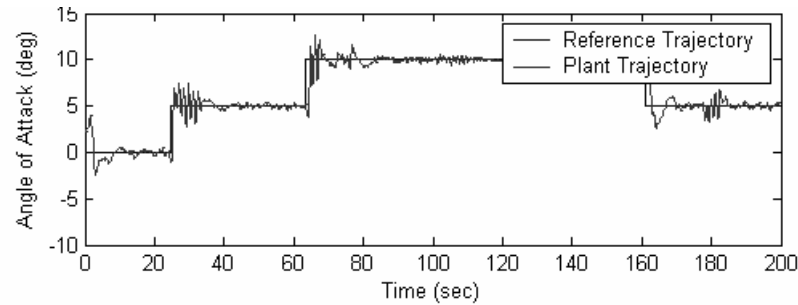


- Good control authority
- Linear !





Demonstration of Pitch Control via Feedback Flow Control





Demonstration of Pitch Control via Feedback Flow Control





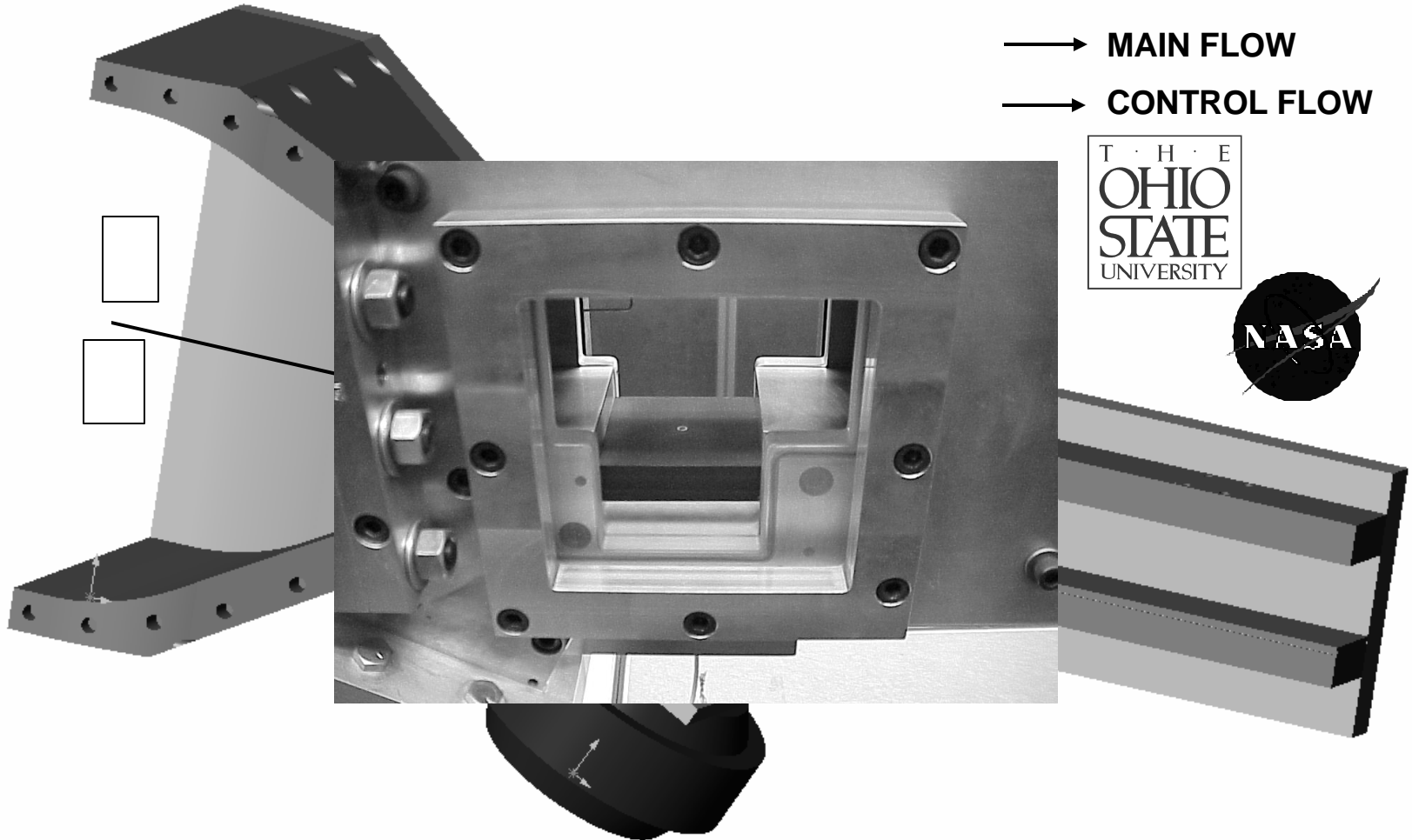
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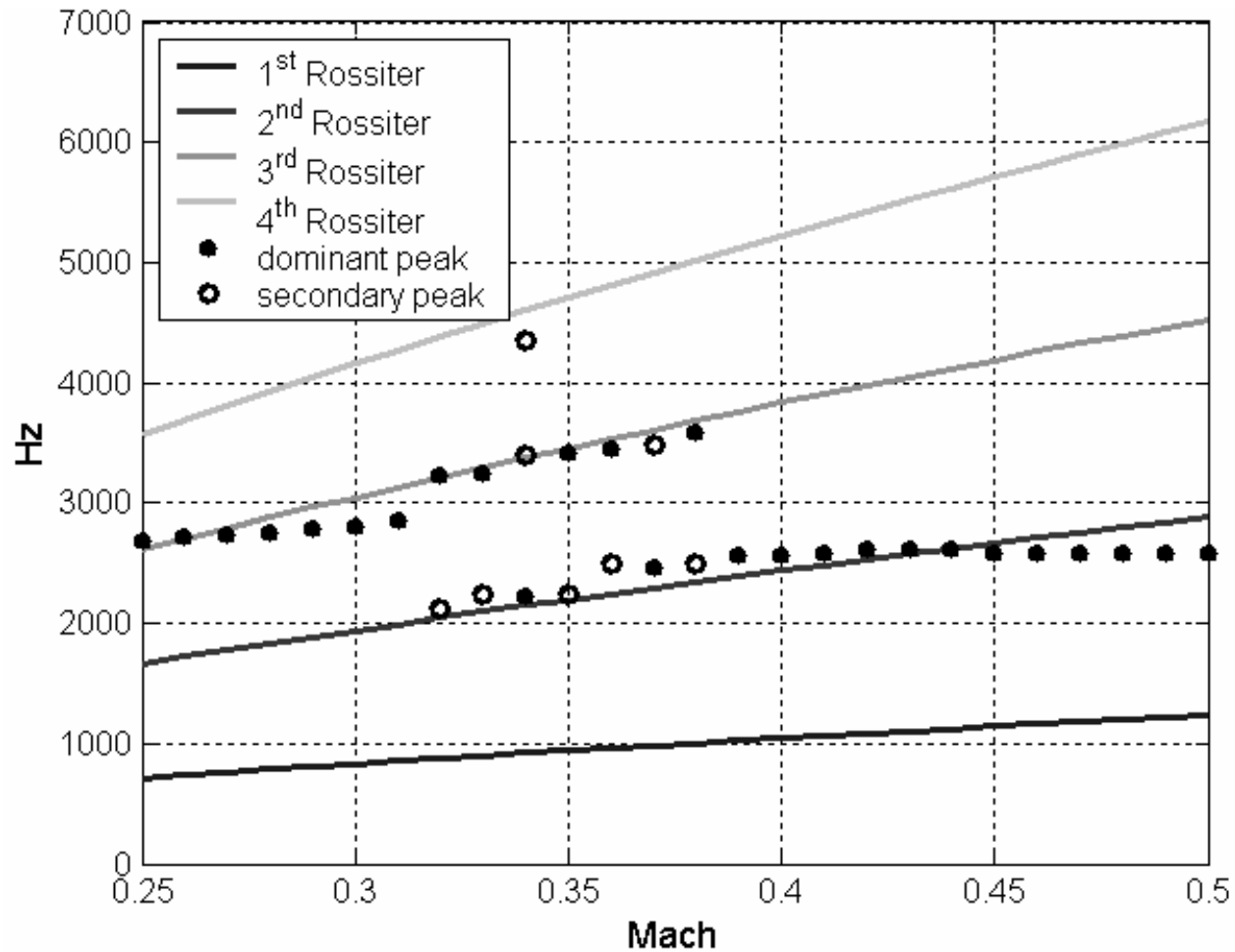


Experimental Arrangement



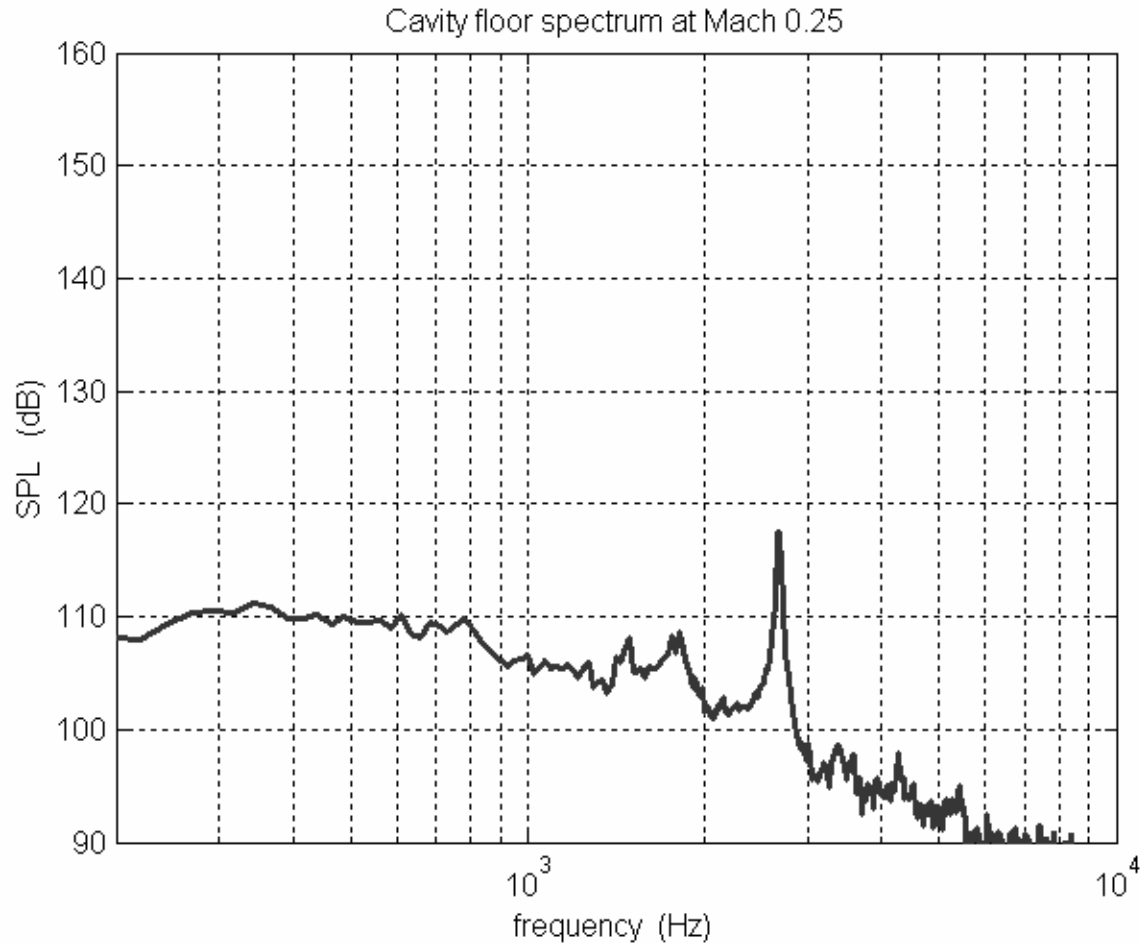


Response Modes





Changing Response w/ Mach

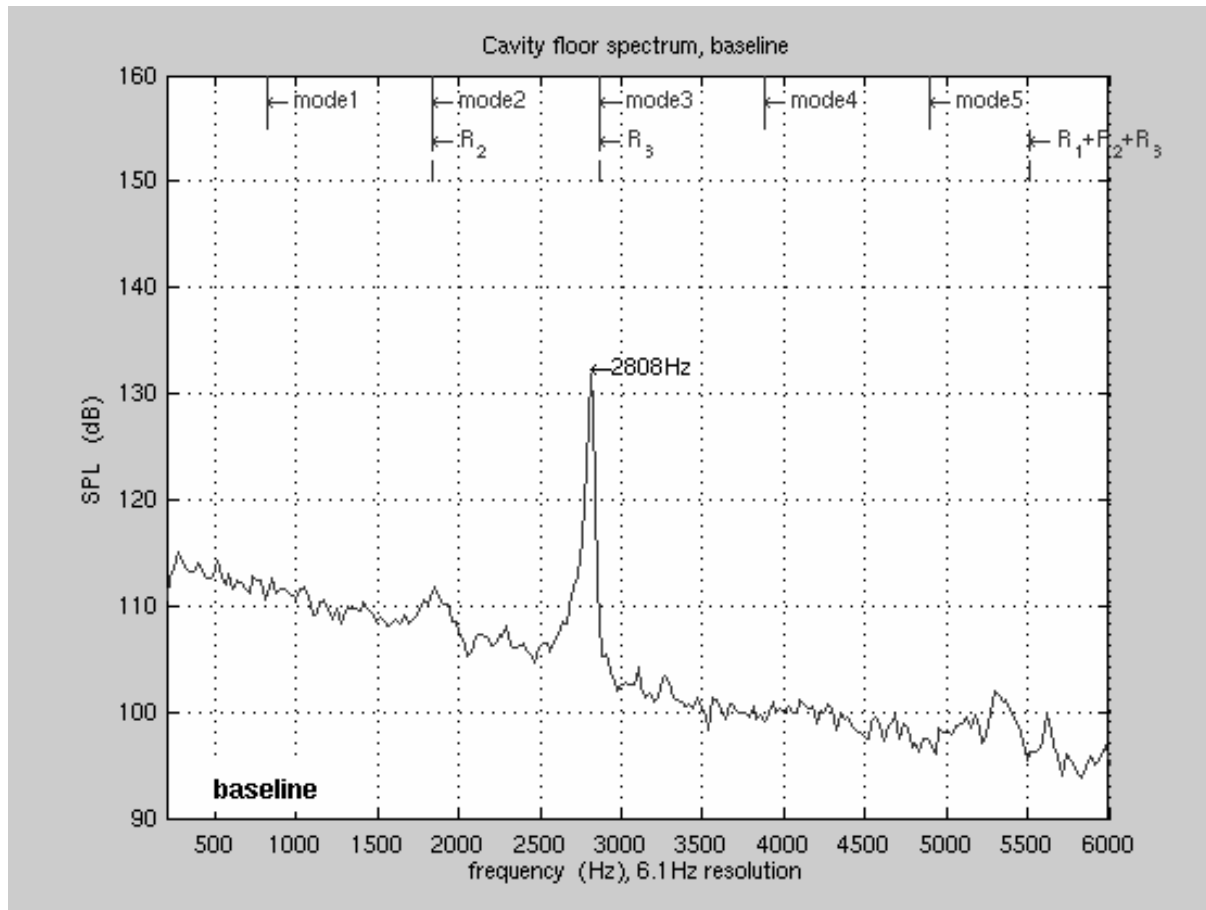




Nonlinearities Lead to Mode-Switching



- Forcing at Frequencies Ranging from 1 kHz to 6 kHz) for Mach 0.30
- Unforced flow exhibits single dominant Rossiter mode

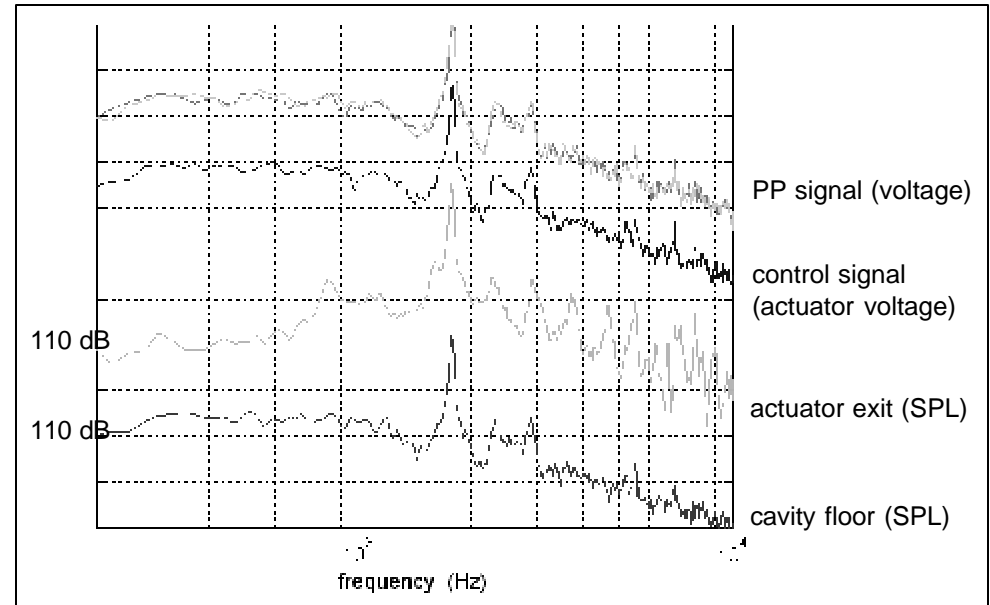
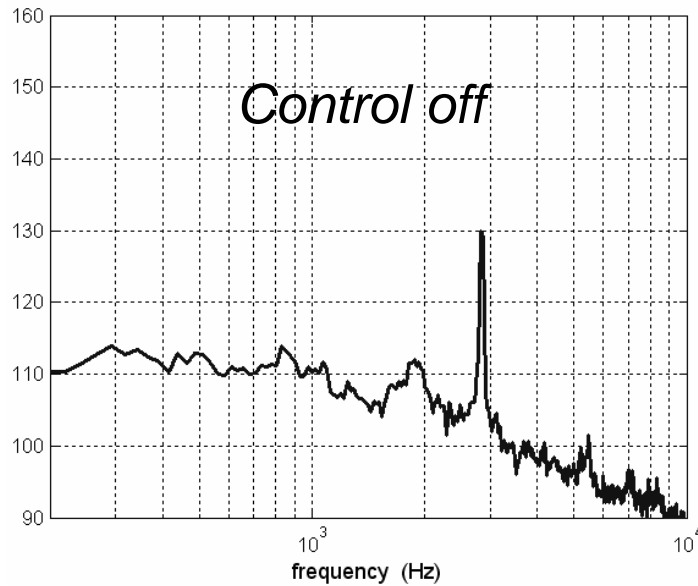
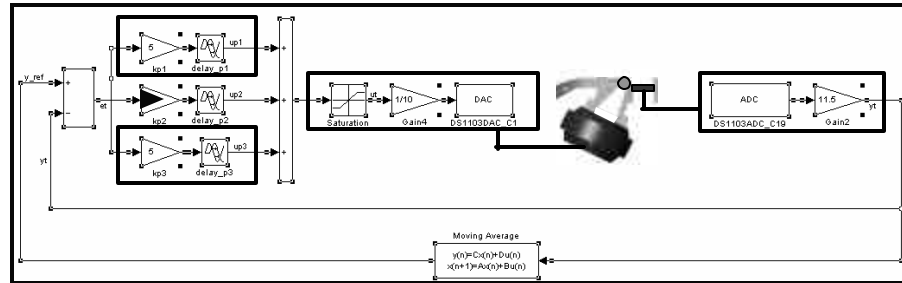




Proportional-Proportional Control



Mach 0.30 flow



2nd Rossiter mode reinforced

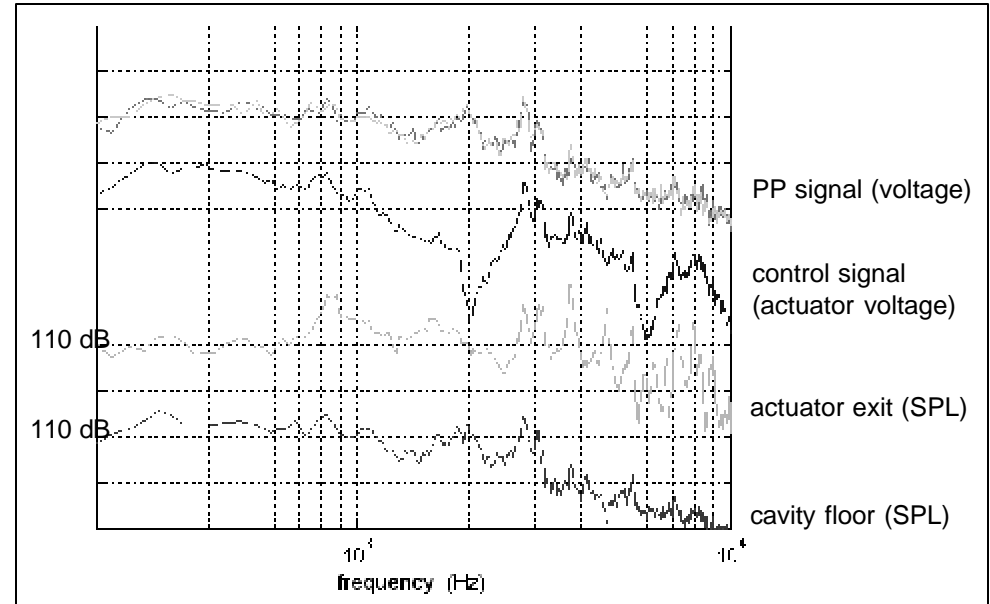
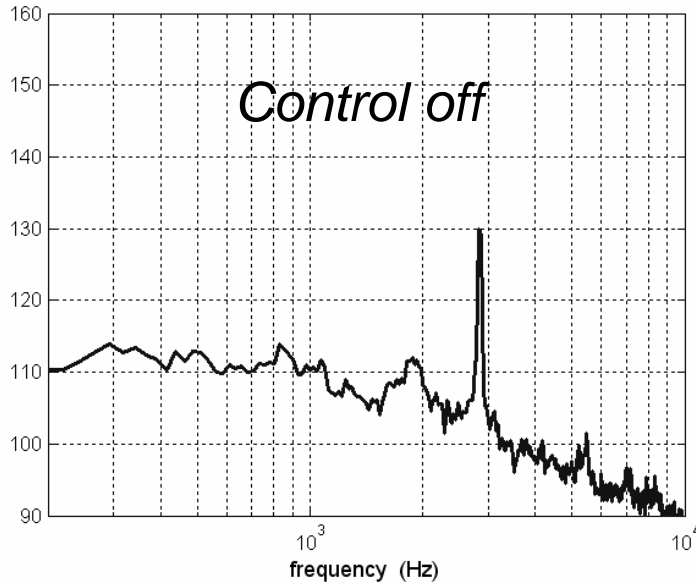
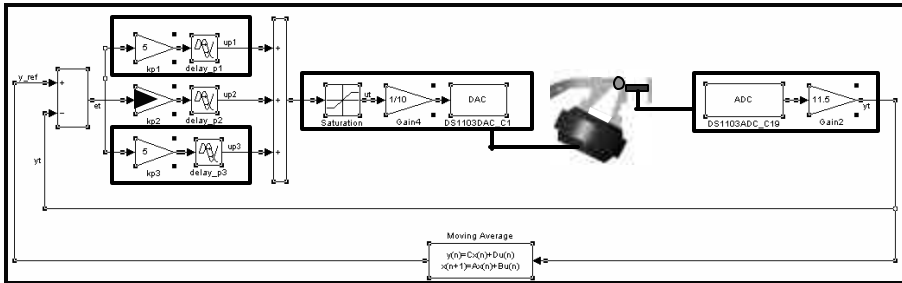


Proportional-Proportional Control



Mach 0.30 flow

Proportional + delayed feedback control
(2 feedback loops out of phase)



Dynamic feedback suppresses resonance

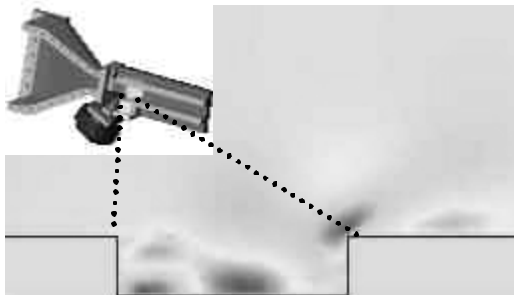
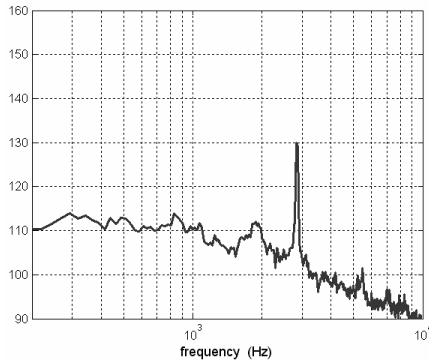


Benefit of Feedback Control Robustness

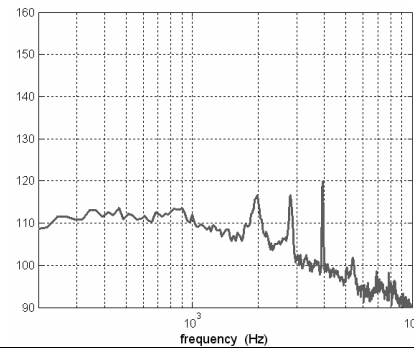
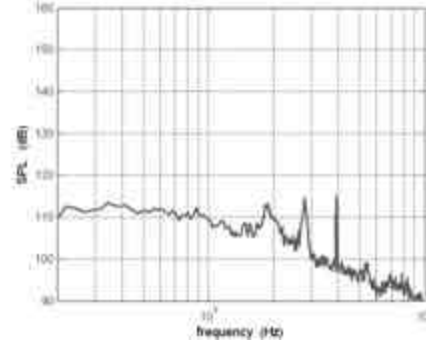
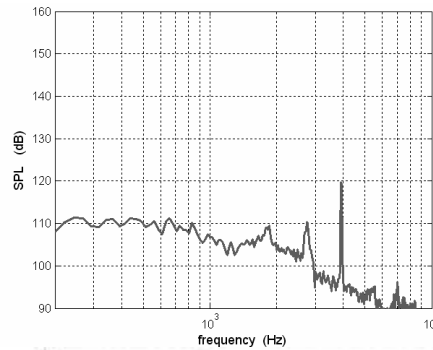


FEEDBACK PRODUCES SUPERIOR RESULTS AT OFF-DESIGN CONDITIONS

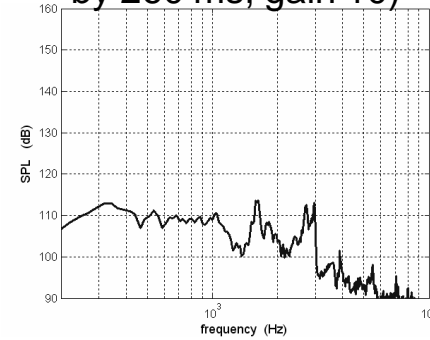
No Control - Mach 0.3



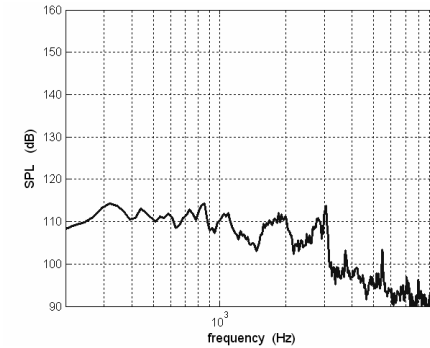
Open-loop Control Optimized for Mach 0.3



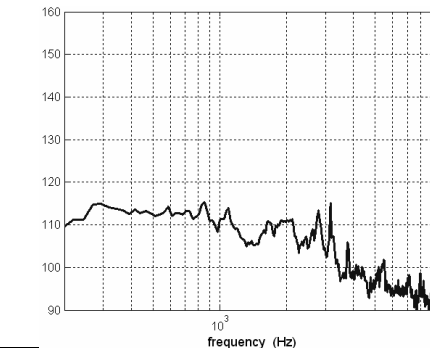
Feedback Flow Control P-P control (P1 leads P2 by 260 ms, gain 10)



Mach 0.27



Mach 0.30



Mach 0.32



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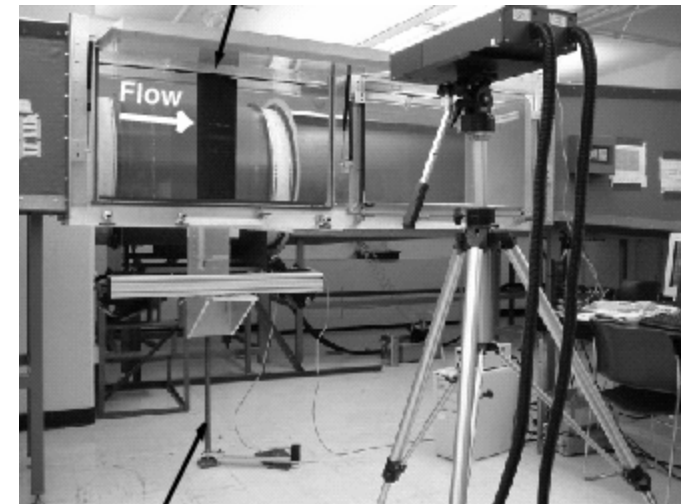
Separation Control on NACA 4412



- **Water tunnel**
 - Laminar flow
 - Simulations for POD model calculation
- **Wind tunnel**
 - Turbulent flow
 - PIV for POD mode calculation
 - 87% of K.E. captured in 50 states
 - mLSM predicts flow separation with 11 surface-mounted pressure sensors



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Demonstration of Feedback Control



NACA 4412 in wind tunnel

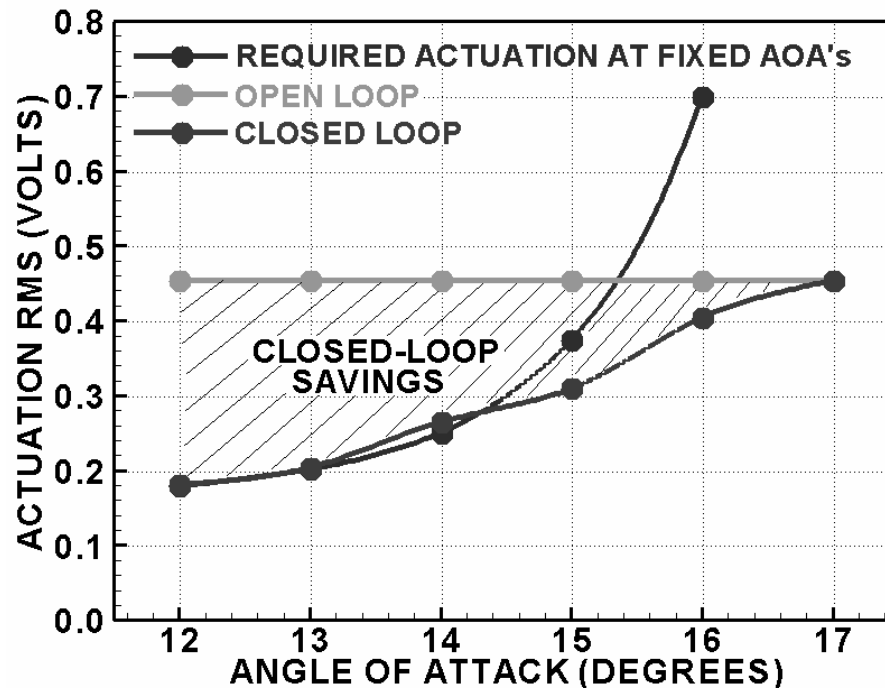




Benefit of Feedback Reduced Power



- Constant pitch rate from 12° to 17° of angle of attack
- Incipient separation at 15°
- Proportional feedback on 1st POD mode which correlates directly to degree of separation



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34% power savings with feedback control



Outline



- **Examples of VA Efforts**
- **What is flow control?**
- **Low-order model approach (KISS)**
 - **Pitching airfoil**
 - **Cavity tone suppression**
 - **Separation control**
- **Reduced-order model approach (KIRS)**
 - **Nonlinear convection**
- **Summary and future work**



Simulation-Based Feedback Flow Control



Benefits:

- Control design and verification before hardware
- Optimal actuator and sensor placement
- Fast investigation of different control formulations

Challenges:

- Simulation time requirements
- Huge system dimension
- CFD and control design often incompatible
- Experimental validation

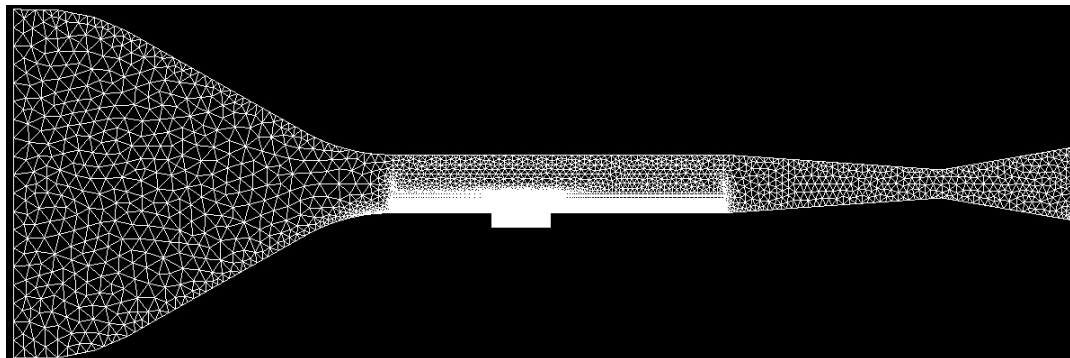


Design/Reduce



Design/Reduce: PDE Feedback Control Design? Discretize

- Issues:**
- **Systematic control formulation (+)**
 - **Control developed with infinite-dimensional model (+)**
 - **Commercial software (+)**
 - **Many open questions for highly nonlinear systems (-)**
 - **Prohibitively expensive gain computation (-)**



63,179 Cells
 $\sim 10^8$ Riccati unknowns

System Structure Can Reduce Computational Expense (AIAA-2004-2411)



Reduce/Design



Reduce/Design: System Model Reduction? Feedback Control Design

- Issues:**
- Low-dimensional system model (+)
 - Fast gain calculation (+)
 - Difficult model development (-)
 - Potentially expensive snapshot generation (-)
 - Potential omission of important dynamics (-)
 - Snapshot control inputs based on intuition (-)

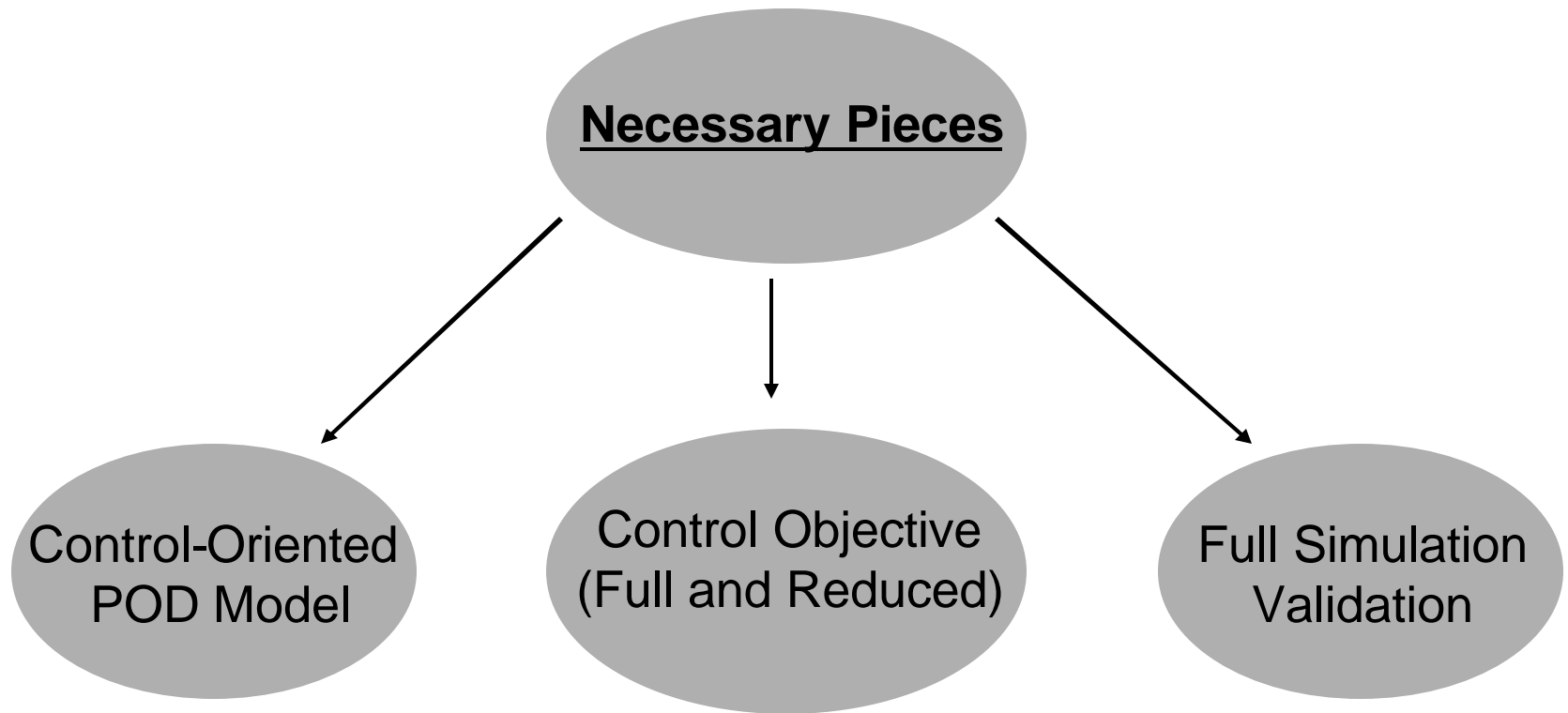
Potential for Tractable Systematic Feedback Flow Control



Proper Orthogonal Decomposition



POD developed primarily as a simulation tool. Can it be used to develop feedback control laws?



Critical Capability: POD Boundary Feedback Control/Verification



Nonlinear Convection Over an Obstacle



Goal: Boundary Tracking Feedback Control

Governing Equation:



**Specify multiple boundary inputs
in snapshot ensemble**

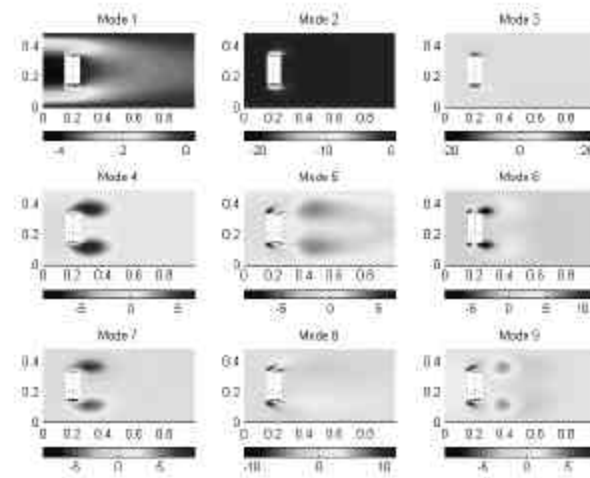
$$u_B(t) = N \sin(0.25t^2) \quad u_T(t) = 0$$

$$u_B(t) = 0 \quad u_T(t) = N \sin(0.25t^2)$$

$$u_B(t) = N \sin(0.25t^2) \quad u_T(t) = N \sin(0.25t^2)$$

$$N = -3, -2, -1$$

First 9 POD Modes

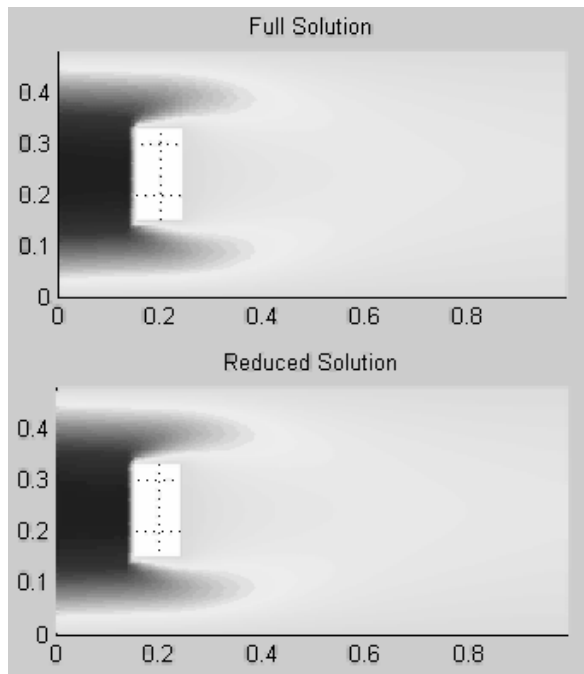




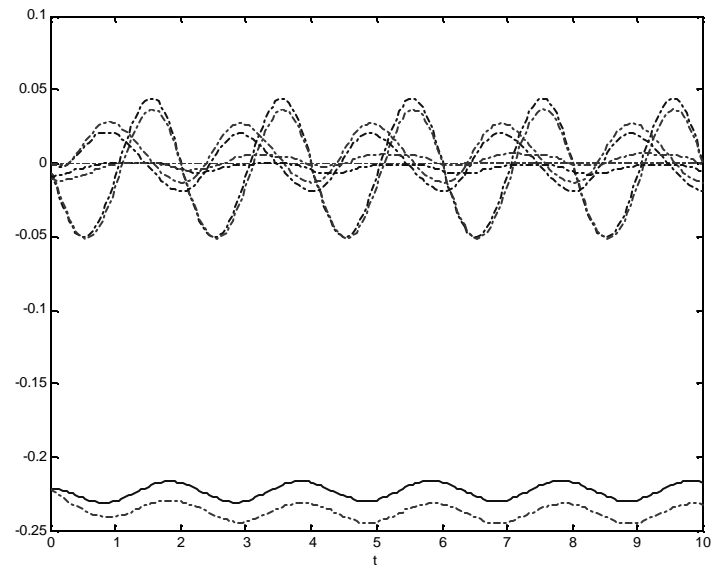
Validate Model

Comparison of POD and Full Order Models

Open-Loop Test



First 5 temporal coefficients



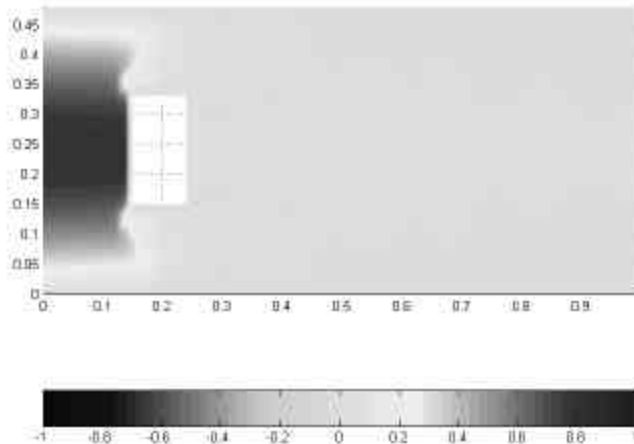


Validate Control Law



Design Control From 25 Modes

Reference Function



Controlled POD Model



Controlled Full Order System



Effective Reduced Control (2005 GNC)

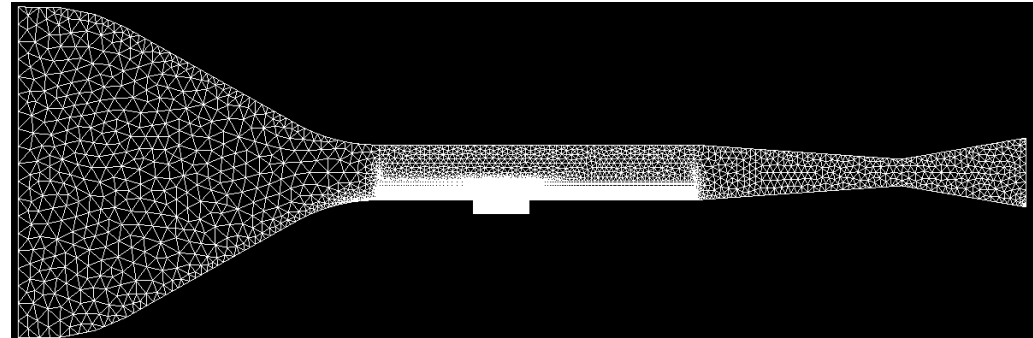


Extension to Navier-Stokes



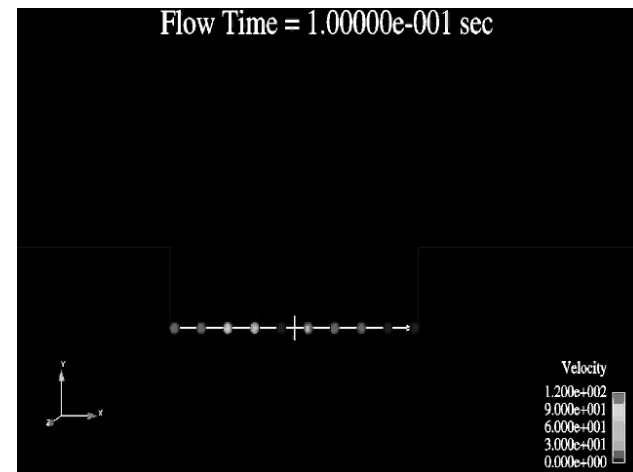
AVUS Flow Solver

- finite-volume, cell centered
- 2nd order accurate in space/time
- CS CoE consultation



Mesh Parameters

- 63,179 Cells
- 43 Cells within boundary layer
- Cavity Resolution
 - 251 streamwise nodes
 - 77 normal nodes





Reduce/Design Conclusions



- **POD Potential for Systematic Boundary Feedback Flow Control**
- **Techniques Developed to Address Critical Issues**
 - **POD basis suitable for range of input conditions**
 - **Reduced models amenable to boundary feedback design**
 - **Control objective for full and reduced systems**
 - **Control-oriented model fidelity**
 - **Full order validation**
- **Methods Tested and Effective**
 - **Heat conduction on cavity geometry**
 - **Nonlinear convection on obstacle geometry**
- **Extending Techniques to Cavity Flow**



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Summary & Future Work



- **Three-pronged approach**
 - **Experiment → Low-Order Model → Control**
 - **Simulation → Order Reduction → Control**
 - **Control → Order Reduction → Experiment**
- **Demonstration of feedback flow control**
 - **Pitch control of 2-D wing in wind tunnel**
 - **Subsonic cavity**
- **Expanding complexity/relevance of problem and robustness/mathematical rigor/generalizability of solution**
- **Future work**
 - **Dynamic pitch/plunge demonstration, flight test**
 - **Application to N-S equations – in-house**
 - **Trade study and flight demonstration**
 - **FY2005 SBIR**

